

EFFECT OF COOLING/LUBRICATION MEDIUM ON MACHINABILITY OF Ti6Al4V

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Abstract: To better understand and know the roles of cooling/lubrication medium in the cutting process and expand their applicability, uncoated cemented carbide tools are used in high-speed turning Ti6Al4V. Dry, cold air, minimal quantity lubrication (MQL), cryogenic MQL, and ionized air as the cooling/lubrication conditions are studied. Experimental results show that at speed 120 m/min turning Ti6Al4V, the cutting force under ionized air is smallest under all lubricant conditions, and tool life is best, next is cryogenic MQL. MQL and cold air almost have the same effect, a little better than dry. Meanwhile the smallest surface roughness is also obtained under ionized air condition. Flank wear and crater wear are the dominant failure modes when high-speed turning Ti6Al4V by SEM analysis. Finally the conclusion is drawn that ionized air and cryogenic MQL have better cooling/lubrication effects and can effectively improve the tool life.

Key words: cooling/lubrication; high-speed turning; Ti6Al4V; minimal quantity lubrication (MQL); ionized air

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INTRODUCTION

Titanium alloys have been widely used in the aerospace, chemical and petroleum industry for good mechanical properties. However, titanium alloys are difficult to machine due to their high temperature strength, relatively low modulus of elasticity, low thermal conductivity, and high chemical reactivity^[1]. High-speed machining technology offers many advantages over conventional machining such as higher material removal rate, increased machining accuracy and better surface finish, etc^[2]. All these advantages have led to the application of high-speed machining technology in titanium alloys^[3].

But severe friction of tool-chip and high cutting temperature lead to rapid tool wear, thereby restricting the processing efficiency^[4]. So a suitable cooling/lubrication medium plays an important role in high-speed machining titanium alloys. Hong et al^[5] injected the focused liquid nitrogen to the chip-tool interface at the point of the high-

est temperature and the flank at the cutting edge through specially designed micro-nozzles, thus effectively improving the tool life. Venugopal et al^[6] utilized the uncoated carbide cutting tool to turn Ti6Al4V alloy, and a substantial improvement in tool life was obtained under cryogenic cooling compared with dry and wet machining. Kovacevic et al^[7] put forward the use of high-pressure water jet cooling to improve surface quality and tool life in the milling of titanium alloy. Yamazaki et al^[8] studied the application of cold air in turning Ti6Al4V and it was proposed that the tool life using cold air was equal to that using minimal quantity lubrication (MQL). The influence of cold air with oil mist on the tool temperature was studied experimentally in the milling of Ti6Al4V alloy^[9]. Su et al^[10] investigated the influence of compressed cold nitrogen gas on tool wear in high-speed end milling of Ti6Al4V and evaluated the effectiveness of cooling/lubrication conditions in tool life.

Static cooling cutting technology is a dry cut-

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ting technology invented by Russian in the eighties of the 20th century, its principle is that the pressed air is ionized by high voltage electric field device, sent into cutting zone through the nozzle, and then a special atmosphere is formed so as to achieve the effects of cooling and lubrication. Rose Technology Company of Russian has done a lot of tests about static cooling technology, and achieved more than thirty national patents. This technology may take the place of the coolant in most situations and succeed to pass the tests in America, Germany, Japan, Switzerland, and other countries^[11]. In China there are a few reports about it^[11-12].

In this paper, uncoated cemented carbide tools are used in high-speed turning Ti6Al4V. Dry, cold air, MQL, cryogenic MQL (CMQL) and ionized air with ozone and oxygen ions as the cooling/lubrication conditions are studied, in order to better understand and know the roles of coolant/lubrication conditions in the cutting process and expand their applicability.

1 EXPERIMENTAL SET-UP

1.1 Workpiece and tool

An $\alpha+\beta$ phase Ti6Al4V alloy is used for the machining tests. The main nominal composition of Ti6Al4V is 90%Ti+6%Al+4%V, with a hardness of HV320—330. YG8, uncoated cemented carbide cutters are used, having rake angle (γ) of -7° , clearance angle (α) of 7° , corner radius (R) of 0.5 mm, and side cutting edge angle (K_r) of 45° .

1.2 Machining tests

All the cutting tests are carried out on CA6140 lathe. The cutting tool is clamped onto the dynamometer. The cutting speed of 120 m/min is chosen to study the effectiveness of various cooling/lubrication conditions in this paper, including dry, cold air (-20°C), MQL, CMQL and ionized air. Feed rate $f = 0.1$ mm/r, and depth of cut $a_p = 0.5$ mm. The temperature of cold air used for CMQL also is -20°C . The experimental set-up of turning as a schematic illustration is shown in Fig. 1.

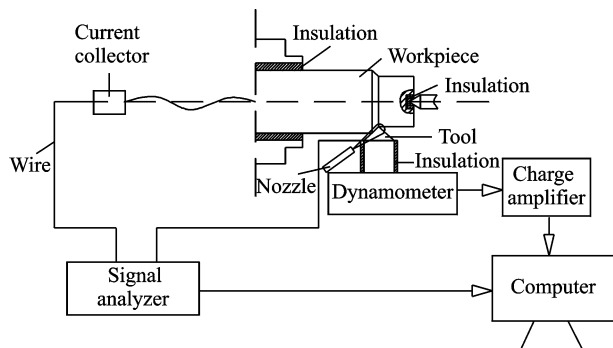


Fig. 1 Schematic illustration of turning set-up

The appropriate lubricant is essential for MQL and CMQL machining. In order to reduce the impact on the environment and simultaneously maintain the performance of lubricant, it also needs to be taken into account that the characteristics of lubricating oil at low temperature, such as viscosity, pour point and so on. In this test, Vascomill MMS FA 1 produced by Blasser Company is used, which is a kind of vegetable oil without chlorine, sulfur or mineral oils, and with the polar molecular structure and fatty alcohol as base oil, and better atomization performance under low temperature. The small amount (30 ml/h) of cutting oil for the mist requirement is supplied at the pressure of 0.4 MPa by external MQL lubrication system VE1B produced by Vogel Company. A nozzle positioned 15 mm away from the cutting tool nose is applied to the rake face.

Ionized air generating device with the dimension of 140 mm \times 100 mm \times 110 mm and the mass of 3.5 kg needs input power 45 W (AC110/220 V, 50/60 Hz), and output voltage is 4.6 kV. It mainly includes high-voltage power supply cell, ion nozzle, wire, and wind-pipe, the diameter of which is 8 mm. After the air is ionized by the ion nozzle, a certain concentration of negative oxygen ions and ozone generated are transported into the cutting zone.

1.3 Measure tools

The cutting forces are measured by Kistler piezoelectric dynamometer 9265B, and the average temperature of the cutting zone is measured using the natural thermocouple method. Surface

roughness of Ti6Al4V is measured using three-dimensional profilometer MicroXAM. Tool rake and flank wears are measured using $10\times$ optical microscope. The worn rake and flank regions on the tools are examined using Joel JSM 5610LV scanning electron microscope.

2 RESULTS AND ANALYSIS

2.1 Cutting force and cutting temperature

Fig. 2 shows the main cutting force F and cutting temperature T under different coolant/lubrication conditions. It is found that under dry condition, the cutting temperature is highest under all conditions, and the cutting force is larger than those under other coolant/lubricants conditions except cold air. MQL has some lubrication action, but little effect at high cutting temperatures for decomposition of the oil film. Cold air cutting has highest main cutting force, but has a better cooling effect, effectively lowering the cutting temperature. CMQL can maintain the stability of lubricating oil film and still play good lubrication action under high-speed cutting conditions, so CMQL has better cooling and lubrication effect for its lowest cutting temperature and smaller cutting force. Compared with that under dry, the cutting temperature under CMQL condition decreases by 14.1%. Ionized air has obvious advantages in reducing main cutting force, which is smallest under all conditions, and decreases by 17.6% than dry cutting.

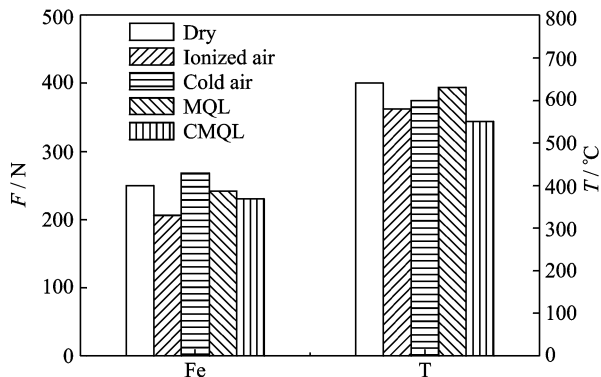


Fig. 2 Cutting force and cutting temperature
($v=120$ m/min, $f=0.1$ mm/r, $a_p=0.5$ mm, $VB=0.1$ mm)

2.2 Tool wear

The results obtained from the cutting experi-

ments show that tool wear is significantly affected by the cooling/lubrication conditions. Fig. 3 shows the curve of tool wear with cutting length L , including average flank wear VB , maximum flank wear VB_{\max} , nose wear VC and rake crater wear KB . When cemented carbide turns titanium alloys, tool wears mainly occur in rake face and flank face. The crater wear in rake face, which seriously weakens the cutting edge, will lead to accelerate the flank wear and the final damage of tool, but intense friction of tool-chip is the main reason of crater wear.

As seen in Fig. 3(a), the flank average wear VB rapidly increases with the cutting length under dry cutting condition, except at a lower rate under other cooling/lubrication conditions, especially when using CMQL and ionized air. CMQL plays an important role in inhibiting the tool wear. In contrast, the effect of ionized air is a little better than CMQL. It is attributed to its antifriction properties, thus effectively reducing the friction of tool-chip. The evidence is that crater wear is the smallest under ionized air condition, as shown in Fig. 3(d). Meanwhile it is found that the maximum flank wear VB_{\max} under dry and MQL conditions are larger than those under other conditions in Fig. 3(b).

Tool wear using cold air is equal to that using MQL. When high-speed turning Ti6Al4V, high cutting temperature makes the oil film break up and the lubrication action lose, so the effect of MQL to improve tool life is not obvious. Cold air can reduce the cutting temperature, expressing a certain advantages at high-speed machining. In Fig. 3(c), the nose wear is most serious under dry cutting condition, which may be the main reason leading to rapid wear of tool. Table 1 shows the wear relative value compared with the tool wear under dry condition, where $v=120$ m/min, $f=0.1$ mm/r, $a_p=0.5$ mm, cutting time $t=8.5$ min. It can be concluded from the results that the wearable performance from worst to best is dry cutting, MQL, cold air, CMQL, and ionized air.

Fig. 4 shows the scanning electron microscope (SEM) images of worn tools under all the

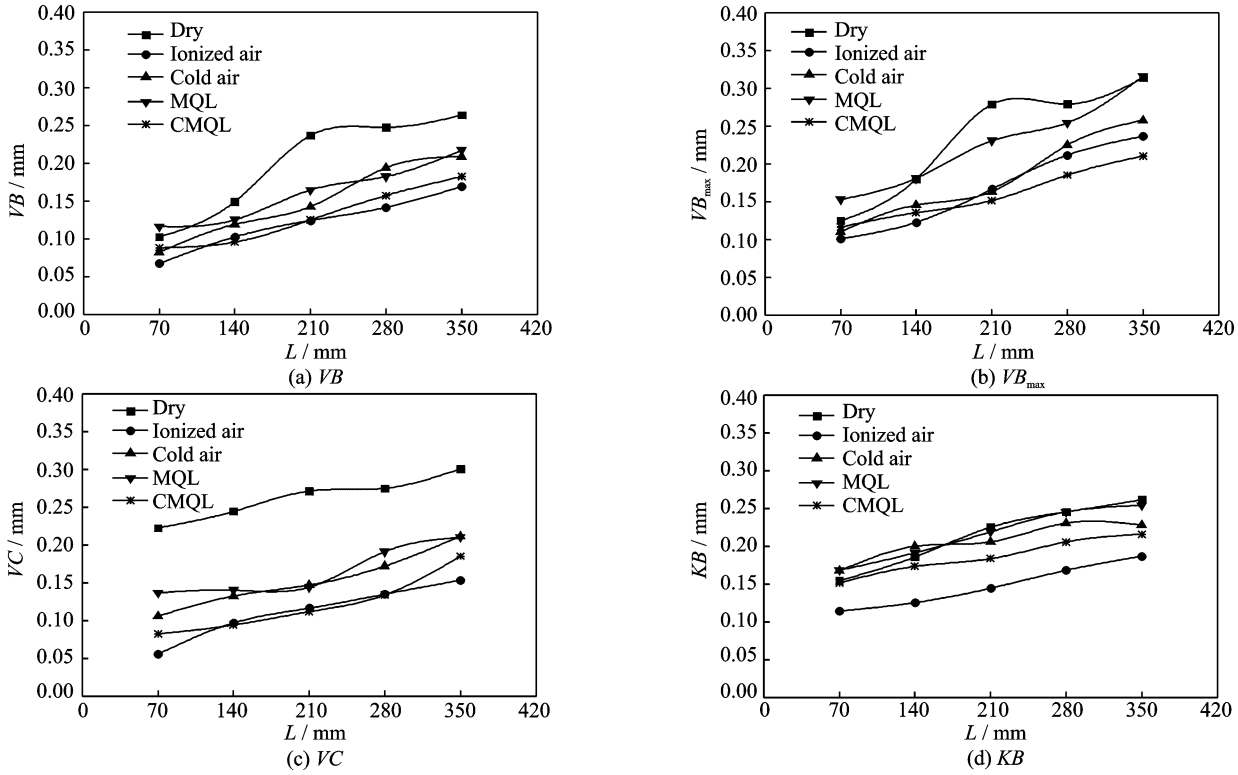


Fig. 3 Tool wears against cutting length

Table 1 Effect of coolant/lubrications on wearable performance

Lubrication condition	VB/mm	Compared wearable performance of flank face	KB/mm	Compared wearable performance of rake face
Dry	0.263 58	1.000 000	0.261 66	1.000 000
Ionized air	0.169 36	1.556 330	0.186 88	1.400 150
Cold air	0.208 74	1.262 719	0.227 85	1.148 387
MQL	0.217 27	1.213 145	0.254 31	1.028 902
CMQL	0.182 28	1.446 017	0.216 09	1.210 884

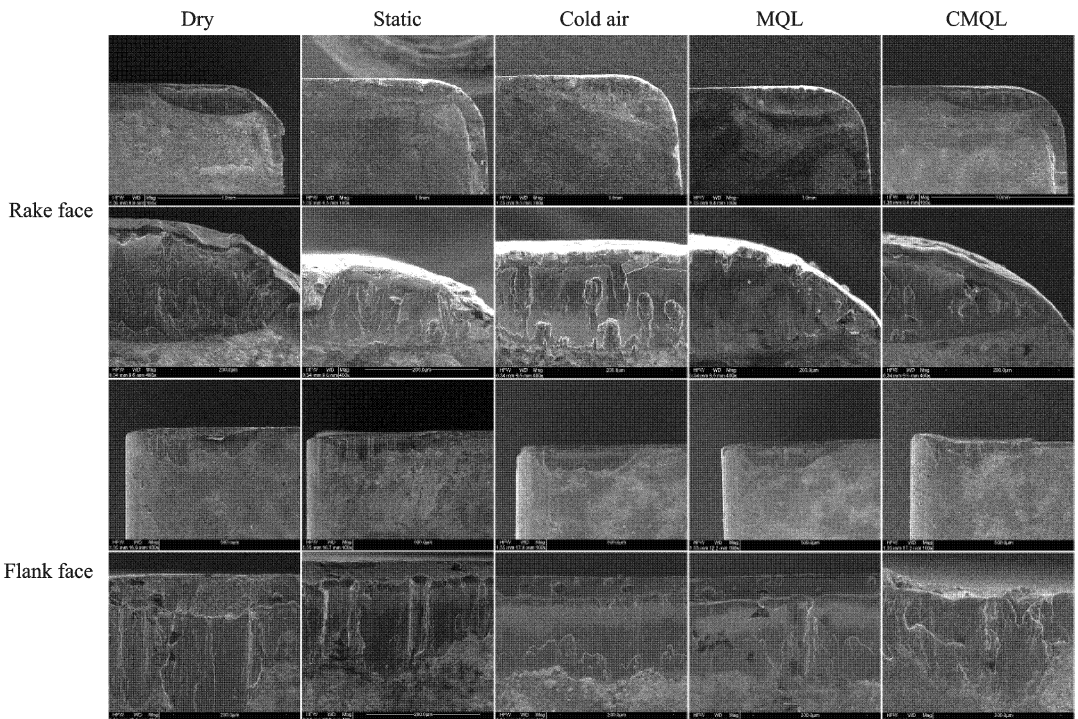


Fig. 4 SEM images of worn tools

coolant/lubrication conditions. Wear mechanisms remain almost the same for all the tools regardless of different conditions. Main modes of tool wear are adhesion wear and chippings.

As seen from Fig. 4, under dry condition, both on the rake and flank, adhesion phenomena are very serious. Meanwhile the cutting edge occurs more chippings under the action of thermal stress. Compared with that under the dry condition, the adhesive materials are less under the CMQL condition. The reason mainly is that cryogenic oil mist reduces the friction between tool and workpiece for its lubrication action, and decreases the temperature for its cooling action, thus reducing the adhesion ability of titanium alloy.

Under the ionized air condition, there are enough high concentrations of ozone and oxygen ions to form oxide films between tool and chip, which put into effect of effective lubrication and anti-friction. The oxide film can prevent the occurrence of adhesion wear. As shown in Fig. 4, crater wear is present in rake face under all the conditions, but smallest in ionized air, which may be the reason of the longest tool life.

2.3 Surface roughness

Fig. 5 illustrates the variation of surface roughness values Ra with the cutting length under different coolant/lubricant conditions. With the increase of cutting length the surface roughness increases slowly but not obviously. And the value of surface roughness under ionized air cooling condition is least under all the conditions. The reason is that under ionized air the Rehbinder effect occurs on the surface of titanium alloy,

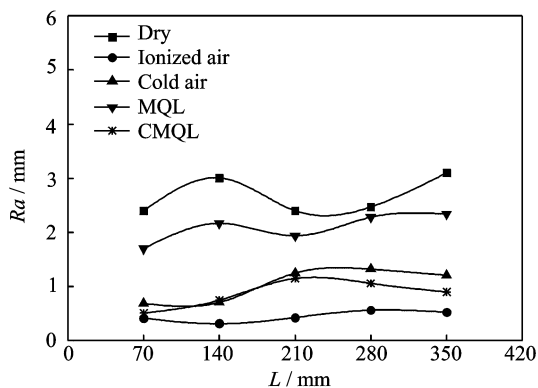


Fig. 5 Surface roughness Ra against cutting time

which is that the surface hardness and strength decrease under the physical and chemical actions as absorbing gas phase particles, surface charging and so on. The internal stress of machined surface is reduced, so the worn surface qualities are improved more effectively.

It is also found that surface roughness Ra under cold air and CMQL conditions are less than that under MQL condition. So in high-speed machining titanium alloy, the cooling effect is better to improve the surface roughness than lubricant effect.

3 CONCLUSIONS

Tests on high-speed turning Ti6Al4V are performed under various cooling/lubrication conditions. Based on the results of test investigation, the following conclusions can be summarized:

(1) Ionized air has obvious advantages in lowering cutting force and can improve tool life and surface roughness when high-speed turning Ti6Al4V. Compared with dry cutting, the cutting force and the tool wear VB under ionized air condition are reduced by 17.6% and 35.7%, respectively.

(2) Cryogenic MQL has good cooling and lubrication actions, and can decrease the cutting temperature by 17.6% and the tool wear VB by 30.8% respectively than dry cutting.

(3) The wearable performance from worst to best is dry, MQL, cold air, CMQL, and ionized air.

(4) Flank wear and crater wear are the dominant failure modes when high-speed turning Ti6Al4V. Ionized air and CMQL can reduce crater wear, thereby inhibiting tool wear rapidly.

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冷却润滑介质对钛合金 Ti6Al4V 加工性能的影响

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摘要:为了更好地理解和认识冷却润滑介质在切削过程中的作用并延伸它们的应用,应用无涂层硬质合金对钛合金 Ti6Al4V 在不同冷却润滑介质下(干切削、冷风、最小量润滑(Minimal quantity lubrication, MQL)、低温MQL 以及电离空气)进行了高速车削试验。结果表明,在 120 m/min 车削 Ti6Al4V 时,电离空气条件下的切削力最小,低温MQL 条件下切削温度最低。电离空气条件下的刀具寿命最长,其次是低温MQL。同时,电离空气条件下获得的加工表面

粗糙度最小。通过扫描电镜分析,高速车削 Ti6Al4V 时,后刀面磨损和月牙洼磨损是刀具磨损的主要方式。实验说明电离空气与低温MQL 具有较好的冷却与润滑效果,可以有效地提高刀具寿命。

关键词:冷却/润滑; 高速车削; Ti6Al4V; 最小量润滑; 电离空气

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