Theoretical and Experimental Investigation of Laser Milling Assisted with Jet Electrochemical Machining

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Abstract: In laser milling assisted with jet electrochemical machining (LMAJECM), the source of energy is a pulsed laser beam aligned coaxially with a jet of electrolyte, which focuses optical energy on the surface of work-piece. The impact of jet of electrolyte develops a state-of-art work to perform operations such as electrolytic etching, effective cooling, and transportation of debris. Therefore, a special jet cell is designed to obtain stable jet as to be a kind of noncontact tool, i. e., electrode. According to the theoretical model of on-off pulse time process, laser machining and electrolytic anodization are simulated by finite element analysis (FEA) method. Grooves on a 0.5 mm thick 321 stainless steel sheet produced by LMAJECM is performed with pulsed Nd: YAG laser at the second harmonic wavelength. Compared with laser milling under ambient atmosphere conditions, the recast layer and burrs are effectively diminished. And the accuracy of depth is dedicated to laser milling, whilst that of width is dominated by jet electrochemical machining. It is demonstrated that LMAJECM can be a highly potential approach for fabricating 3-D micro components.

Key words: micromachining; laser milling; jet electrochemical machining; recast layer

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1 Introduction

Micromachining processes have been found widespread use in a variety of applications in mechanical and biomedical devices. With the development of mechanical science, the three-dimensional (3-D) components need to be manufactured with low cost, high accuracy and high quality surface finishing^[1-3].

Laser beam machining (LBM) has been widely used as a powerful tool in the micro scope machining process, such as cutting^[4-5], drilling^[6-8], welding^[9-11], shock processing^[12], cladding^[13-14] and milling^[15-17]. Laser milling consists in an ablation operation causing vaporization of material as a result of interaction between a laser beam and a machined workpiece. Laser milling

can be applied to a wide range of materials and allows the production of complex shape parts without expensive tooling. Compared with conventional micro-machining processes, laser milling is a non-contact material removal process, which involves highly localized heat input to the workpiece, thus minimizing distortion. It also offers no tool wear. Therefore, laser milling is not limited by constraints such as the maximum tool force, buildup edge formation, or tool chatter. However, laser milling has a number of inherent defects, including recast layer and spatter, which are likely to affect the surface quality.

Jet electrochemical machining is a useful micro machining process without shaped cathode. A hybrid process of jet electrochemical machining and laser beam machining (JECM-LBM) has been

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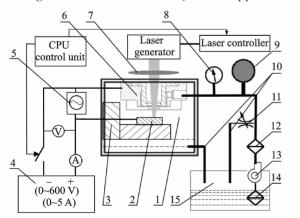
developed to reduce recast layers and spatter effectively[18-22]. JECM-LBM combines two different sources of energy simultaneously, i. e., the energy of photons and the energy of ions. The main aim of combining a jet electrolyte with laser beam is to obtain high process quality by reducing the recast layer and spatter produced in laser beam machining. The jet electrolyte is coaxially aligned with a focused laser beam and creates a noncontact tool-electrode. The focused laser beam and the jet electrolyte act on the same surface of workpiece synchronously. Material is removed mainly by laser beam machining and the defects are overcome by the multiple effects of jet electrolyte, i. e., the effective cooling to workpiece, the transporting debris and the electrochemical reaction with materials, JECM-LBM has been successfully applied to hole-machining.

In this research, based on the JECM-LBM, a new micro-machining process of laser milling assisted with jet electrochemical machining (LMAJECM) has been developed to obtain high accuracy and high quality surface finishing.

2 Experimental Procedures

2. 1 Experimental apparatus

Fig. 1 shows an LMAJECM apparatus,

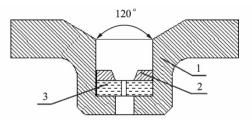


1—Machining chamber; 2—Workpiece; 3—CNC Table; 4—DC power supply system; 5—Oscilloscope; 6—Jet cell; 7—Focusing lens; 8—Pressure gauge; 9—Accumulator; 10—Back pipelines; 11—Pressure regulating valve; 12—Secondly filter; 13—Pump; 14—First filter; 15—Electrolyte reservoir.

Fig. 1 System schematic diagram of LMAJECM

which consists of three systems, namely, a laser system, an electrolyte supply system and a power supply system. A jet cell is placed coaxially with the focused laser beam. An electrolyte is pumped from a reservoir and flows into the jet cell forming a jet of diameter 0.4 mm. The jet and the focused laser beam act on the same surface of workpiece synchronously. The electrolyte jet pressure can be controlled by a pump with pressure varying from 0.3 MPa to 1.5 MPa.

The key part of the jet cell is a nozzle, as shown in Figs. 2, 3. The material and design of the nozzle are important to the concentration of electrolyte and stable jet formation. Ruby is a good material for nozzle with high hardness, good wear resistance and chemical stability, hence, ruby nozzle is a core component. In order to obtain a stable and coherent jet of electrolyte, a conical design is developed for the cavity of nozzle.



1—Base; 2—Copper sleeve; 3—Ruby nozzle.

Fig. 2 Nozzle structure

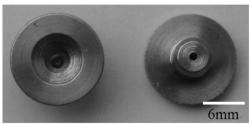


Fig. 3 Photo of nozzle used in the experiment

2.2 Experimental parameters

The experiments of LMAJECM were conducted using a pulsed Nd: YAG laser with the second harmonic wavelength, which can emit a green laser with wavelength of 532 nm. Pulse length of the used laser is 0.2 ms and its frequency is 1 Hz. Energy per pulse is in the range of 300 mJ. The laser beam was focused using a lens of focal length 100 mm. The DC power supply volt-

age used in this paper is 300 V. The concentration of NaNO₃ electrolyte is 15% and pressure is 0.8 MPa. The distance between the nozzle and workpiece is 2 mm. The workpiece is a 1Cr18Ni9Ti stainless sheet with the thickness of 0.5 mm. Sodium nitrate electrolyte with a concentration of 18% by weight is used for the experiments. The conductivity of the electrolyte is $12.2~(\Omega \cdot m)^{-1}$ and the volume electrochemical equivalent of 321 stainless is $2.1\times10^{-9}~m^3/A \cdot min$. The current efficiency is about 60%.

3 Theoretical Model of LMAJECM

3.1 Theoretical analysis

There are two processes in LMAJECM. One is laser action, and the other is electrochemical action. In laser pulse width (T_1) , the laser action is the main role to remove material; while in laser inter-pulse (T_2) , materials are removed by the electrochemical action. The two processes are repeated alternately. The main idea for the theoretical analysis is presented in Fig. 4.

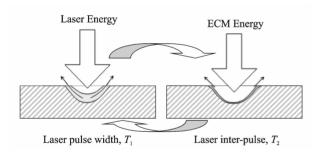


Fig. 4 Energy used for LMAJECM

3.2 FEM modeling

The temperature field with pulse laser in T_1 and the electrochemical field with jet electrochemical machining in T_2 are simulated by finite element method (FEM) software ANSYS. The current temperature field and electrochemical machining field are separately calculated in time domain. During the T_1 , a section profile of processing zone with laser action can be calculated. Then the section profile becomes the initial boundary for the electrochemical machining during the T_2 . When T_2 is ended, the result of section profile will become the initial boundary for laser action in T_1 in the next step. Therefore, in two-dimensions

sional (2-D) space domain, the results of laser action and electrochemical machining are added till the machined time is ended.

Fig. 5 shows the simulation results of temperature field on the workpiece surface with laser pulse energy of 200 mJ in the first T_1 time. It clearly shows the distributions of the workpiece internal temperature with laser drilling process, in which the temperature reached 10 000 $^{\circ}$ C, far exceeding the melting point and boiling point of stainless steel material. Therefore, the elements whose temperature is higher than melting point can be deemed to be removed. The left element boundary can be seen as the initial boundary for electric filed with jet electrochemical machining. Fig. 6 shows the boundary graph after the first laser action.

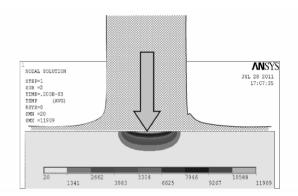


Fig. 5 Temperature field distribution at pulse width

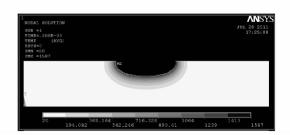


Fig. 6 Boundary graph after the first laser action

Fig. 7 shows the electric field distribution and current density distribution in pulse inter. It can be seen that the current density in the hole at the center of the bottom is about 80 A/cm². Moreover, with the incensement of radial distance, the current density increases rapidly. On the boundary, the current density gains its maximum value, up to 270 A/cm² approximately. Therefore, as the dissolution rate is high, with increasing radial

distance, the current density decreases and the dissolution rate of materials has also been slowed down.

4 Experimental Results

Compared with laser milling in air, the millisecond green laser has been used to machining a groove with LMAJECM. The energy per pulse is 200 mJ, and the electrochemical machining voltage is 300 V. An optical microscope is used to de-

tect the experimental results.

In Fig. 8, the surface of groove with laser drilling in air, both sides are encircled with large areas of irregular spatter deposits. In contrast, it is evident from Fig. 9 that little spatter is presented around the groove machined with LMA-JECM. The most probable reason for this is the presence of the high-speed jet electrolyte, which can effectively cool the ejected material and carry debris away.

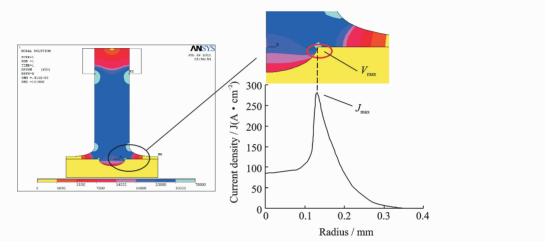


Fig. 7 Distribution of electric field and current density in the inter pulse

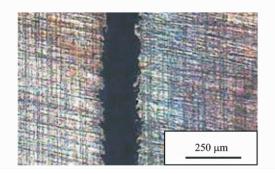


Fig. 8 Groove machined with laser milling in air

Figs. 10,11 show further details of the profile of groove machined with different methods respectively. Unlike the case of laser milling in air, the side-walls of the grooves machined with LMAJECM in Fig. 11 shows that neither spatter nor recast can be observed. There are a large number of recast layers on the side-walls of grooves machined with laser milling in air. The boundary between the recast layer and base material is obvious. The recast layer on the upper part of side-walls is thick and the thickness is about 45

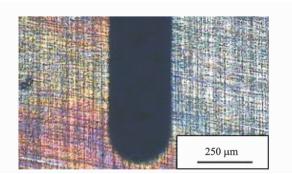


Fig. 9 Groove machined with LAJECM

μm. The recast layer on the lower half part of side-walls is thinner than that on the upper. The phenomenon can be explained by the fact that the bottom material melts and sprays outward with high speed under the high pressure generated by laser action. However, when the melted material is injected into half part of side-walls, the pressure is low. Fig. 12 shows the case of a special 3-D shaped groove machined with LAJECM. It can be proved that LAJECM is an effective micromachining approach.

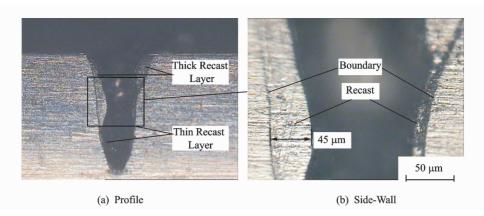


Fig. 10 Laser milling in air

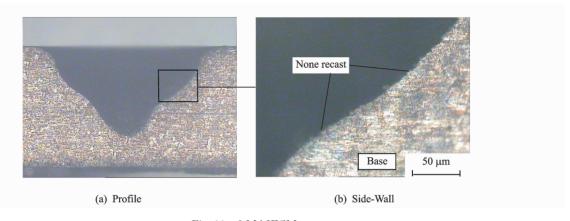


Fig. 11 LMAJECM

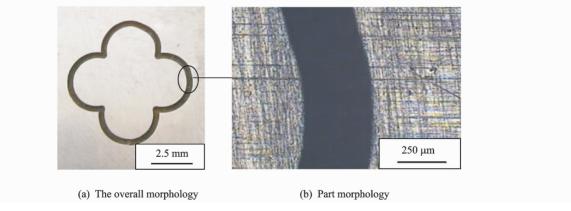


Fig. 12 Special shaped groove machined with LMAJECM

5 Conclusions

The main conclusions can be summarized as follows:

- (1) A special jet cell has been designed for obtaining a stable jet being aligned coaxially with a focused laser beam and creates a noncontact tool-electrode.
- (2) The simulated results of LMAJECM with FEM software show that the groove depth

and width are dominated by the laser and the jet electrochemical machining, respectively.

- (3) Recast and spatter are effectively reduced during the hybrid process of LMFAJECM.
- (4) Materials are removed by the composite action between laser action and electrochemical action during LMAJECM. The electrochemical machining is an auxiliary effect to reduce the recast and spatter effectively.
 - (5) With the further study on the machined

accuracy with section size for LMAJECM, the new process may be a useful machining way for 3-D component micro-machining.

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